

Copyright © IJCESEN

International Journal of Computational and Experimental Science and ENgineering (IJCESEN)

Vol. 11-No.1 (2025) pp. 435-439 <u>http://www.ijcesen.com</u>



Research Article

Modeling of thermal stresses on steel beam

Naim Syla¹, Fisnik Aliaj², Arbër Zeqiraj³ and Bashkim Dalipi ^{4*}

¹University of Prishtina, Department of Physics, Eqrem Çabej Str. 51, 10000 Prishtina, Republic of Kosovo E - mail: naim.syla@uni-pr.edu - ORCID:0000-0003-0857-4685

²University of Prishtina, Department of Physics, Eqrem Çabej Str. 51, 10000 Prishtina, Republic of Kosovo E - mail: fisnik.aliaj@uni-pr.edu - ORCID:0000-0002-9967-8334

³University of Mitrovica, Faculty of Geosciences, Ukshin Kovaçica, Str. 40000 Mitrovica, Kosovo E - mail: arber.zeqiraj@umib.net - ORCID:0000-0002-8615-6641

⁴Public University Kadri Zeka, Faculty of Education, rr."Zija Shemsiu" pn. 60000 Gjilan, Republic of Kosovo * Corresponding AuthorEmail: bashkim.dalipi@uni-gjilan.edu - ORCID:0000-0002-8133-0452

Article Info:

DOI:10.22399/ijcesen.767 **Received:**13 December 2024 **Accepted:**12 January 2025

Keywords:

Modeling, Steel, Heat, Thermal stress, Temperature field, Structure field.

Abstract:

If the edges of a metal structure are subjected to a temperature difference, then because of the temperature gradient in the metal, thermal stresses will appear. To address this phenomenon, we will take the example of a steel beam, which is part of a metal construction. The geometry of the beam is regular and one end of it is subjected to a continuous emission of heat (for example, it is close to the oven) while the other end is in contact with the surrounding external environment. For simplicity, we will assume that the heat emission is constant, so the temperature of the edge of the beam is also constant. Likewise, for the temperature of the other end, we will assume that it is constant. Let the temperature of the first end be T_i , while that of the second end is T_i , then the difference $\Delta T = T_i - T_i$ causes the flow of heat, respectively the occurrence of thermal stresses. Mathematically, heat flow is described by a differential equation in the temperature field, while the functional dependence of the deformation is described by a differential equation in the field of structures - Hooke's law. So, we have two differential equations from two fields: thermal and structural. We have solved them with the finite element method in temperature-structure coupled field, while the simulation in ANSYS (ANSYS is a comprehensive engineering simulation software that is widely used for finite element analysis (FEA), computational fluid dynamics (CFD), and other simulation tasks.). The algorithm of the FE (Finite Element) method and the simulation in ANSYS prove that the treatment can be done for other integration conditions (geometry, material and different temperatures).

1. Introduction

Experience shows us that, when a metal construction is subjected to temperature changes, it is deformed (Figure 1) and in special cases even destroyed (Figure 2) [1].

To eliminate these consequences, when a metallic construction is subjected to temperature changes, then usually an empty space is left in the places where the metals are joined (Figure 3). The reason for the deformation or the destruction of the metal constructions is thermal stress. Thermal stress is the stress produced by any change in the temperature of the material in our case metal [2]. Thermal stress is induced in a metal construction when the

temperature of the metal is raised or lowered, and the construction is not allowed to expand or contract freely. Thermal stress includes both heat and cold stress.



Figure 1. Warped rails.



Figure 2. A broken metal beam.



Figure 3. Example of joining two metals plates on a bridge.

2. Theory of thermal stress

If the metal beam is subjected to a change in temperature, then it shrinks (for the case when it cools) or extends (for the case when it heats up), figure 4. Let l_i be the length of the metallic beam at the initial temperature t_i , while at the final temperature t_f , we

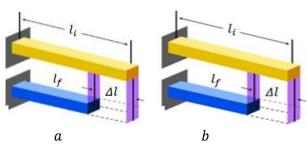


Figure 4. Changing the length of the metal beam for the case when it cools (a) and for the case when it heats up (b).

will mark the length of the beam with l_f . The change in the length of the beam will be [3]:

$$\Delta l = l_f - l_i = \alpha l_i \Delta t$$

where is

$$\Delta t = t_f - t_i$$

and α is the coefficient of thermal expansion of metal in unit 1/K.

For the case when $\Delta t = t_f - t_i > 0$ we will take $\Delta l = l_f - l_i => 0$ and for the case $\Delta t = t_f - t_i < 0$ we have $\Delta l = l_f - l_i < 0$.

In the first case, we say that during heating, the beam lengthens, while in the second, during cooling, it shrinks.

The beam strain will be [3],

$$\varepsilon_t = \frac{\Delta l}{l_i} = \alpha \Delta t$$

We have marked the strain with the index t to show that it depends on the temperature.

Based on Hooke's law, for thermal stress we will get,

$$\sigma_t = E \cdot \varepsilon_t = E \cdot \alpha \Delta t$$

E is Young's Modulus in unit $\frac{N}{m^2}$. From the last equation, it follows that the thermal stress σ_t also has the same unit of measurement $\frac{N}{m^2}$.

2.1 Investigation of thermal stresses

Of practical interest is the assessment of thermal stress. Many authors in their publications explain the ways of experimental evaluation of these stresses [4]. Well, for us in this paper the most important thing is the theoretical approach of recognizing and evaluating thermal stress. One of the most popular theoretical methods is the Finite Element Method (FE Method). There are many well-known treatments of thermal stress according to the FE Method. One of the known examples is the treatment of thermal stress in the sheet metal of the dome of the Church of Our Lady in Dresden (Figure 5) [5,6].

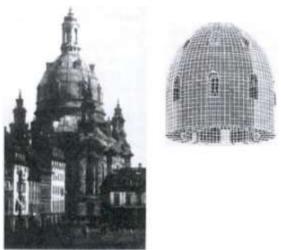


Figure 5. Model of the dome of the church of Our Lady according to the FE Method.

Usually, the models built according to the FE method are supported by the ANSYS application, which enables the recognition and evaluation of the thermal stress components [5, 6].

3. Modeling and results

The above example, we have treated according to the Fe method in the coupled mechanical-thermal field. According to this method, the matrix forms in the temperature respectively mechanical fields are, [6,7].

$$[\lambda] \cdot \{T\} = -\{Q\} \; ; \; [k] \cdot \{u\} = \{F\}$$

Where are:

- $[\lambda]$ conductivity matrix
- $\{T\}$ vector of o temperatures at the nodes
- {Q} vector of heat flow in the nodes
- [k] stiffness matrix
- {u} vector of nodes displacement and
- {F}- vector of force in the nodes.

The complete equation of the couple fields' temperature structure is:

$$[k_t] \cdot \{u_t\} = \{F_t\}$$

Where

$$[k_t] = \begin{bmatrix} \lambda & 0 \\ 0 & k \end{bmatrix}, \{u_t\} = \begin{Bmatrix} u \\ T \end{Bmatrix}$$
 and $\{F_t\} = \begin{Bmatrix} F \\ Q \end{Bmatrix}$

We have proposed a model with regular geometry with dimensions 0.5mx0.6mx10m (Figure 6) and constructed of steel. The physical characteristics of steel are thermal conductivity coefficient $\lambda = 45 \text{ W/m} \cdot \text{K}$ [6] modulus of elasticity $E = 210000 \cdot 10^6 \text{ N/m}^2$, [7] linear expansion coefficient $\alpha = 12 \cdot 10^{-6} \cdot \frac{1}{\text{K}}$ [6] and Poisson's ratio v = 0.3 [8].

Let these be the integration conditions: for z=0, the temperature is $t_i=20\,^{\circ}\text{C}$, while for $z=10\,\text{m}$, let the temperature be $t_f=100\,^{\circ}\text{C}$. We will assume that the temperature difference between the ends of the beam is constant $\Delta t=t_f-t_i=80\,^{\circ}\text{C}=80\,K$. While, as far as the mechanical conditions are concerned, we assume that for z=0 all the degrees of freedom are fixed, while for z=10m, only the degree of freedom y is fixed (the others are not because the beam can swell), (Figure 7). For these integration conditions and physical and geometric characteristics of the sample, the program was

written in APDL [6]. The required solutions are the thermal stress distributions along different directions (Figure 8). As a result of the temperature difference, we have a flow of heat which causes the deformation of the crystal lattice of the metal and as a result, thermal stresses appear σ_t . To know the distribution of the thermal stress intensity along the length of the beam, according to the Fe Method, we must calculate the components of σ_t [9]

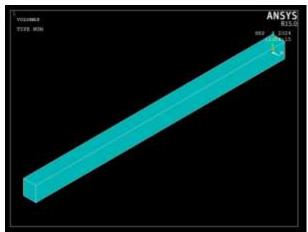


Figure 6. The model in the workbench of ANSYS.

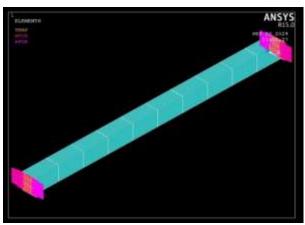


Figure 7. Conditions of integration in the model.

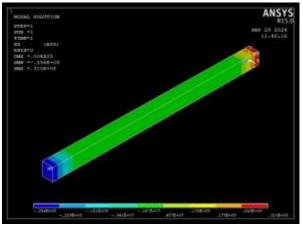


Figure 8a. The distribution of stresses along the axis z.

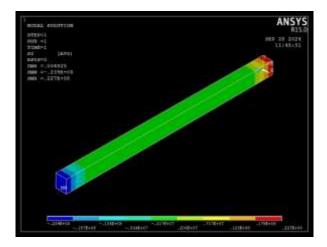


Figure 8b. The distribution of stresses along the axis y.

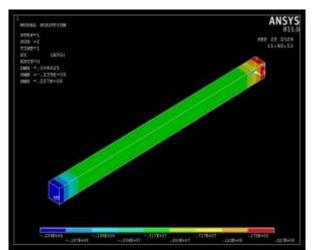


Figure 8c. The distribution of stresses along the axis x.

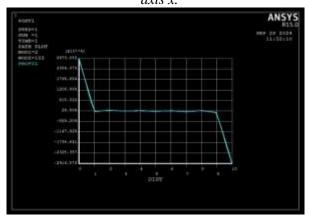


Figure 9. Profile s(z).

$$\sigma_t = \begin{cases} \sigma_1 \\ \sigma_2 \\ \sigma_i \\ \sigma_{n-1} \\ \sigma_n \end{cases}$$

Where $\sigma_1, \sigma_2, \dots \sigma_i, \dots, \sigma_n$, are the components of the vector σ_t at nodes i.

and finally, in figure 9, we will present the distribution profile of the intensity of stress along the z axis [10]. It should also be noted that there a number of works done on steel and reported [11-16]. Based on the above text and the results (simulations), we can conclude the following:

- Thermal stress can be modeled with the FE method
- Thermal stress is modeled in the coupled fields' temperature structure
- Modeling is supported by the ANSYS software
- In the same manner, other cases can also be modeled (materials and other integration conditions)

Author Statements:

- **Ethical approval:** The conducted research is not related to either human or animal use.
- Conflict of interest: The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper
- Acknowledgement: The authors declare that they have nobody or no-company to acknowledge.
- **Author contributions:** The authors declare that they have equal right on this paper.
- **Funding information:** The authors declare that there is no funding to be acknowledged.
- **Data availability statement:** The data that support the findings of this study are available on request from the corresponding author. The data are not publicly available due to privacy or ethical restrictions.

References

- [1] Geogreta Baeatu et al. (2017). Behavior of Steel Structures under Elevated Temperature. *Procedia Engineering* 181(15-16):265-272. DOI:10.1016/j.proeng.2017.02.388.
- [2] Bhausaheb R.Sontakke et al. (2021). Study of thermal stress analysis. *Journal of the Maharaja Sayajirao University of Baroda* 55(1).
- [3] Hemangi K. Patade, Dr. M. A. Chakrabarti. (2013) Thermal Stress Analysis of Beam Subjected To Fire. Int. Journal of Engineering Research and Application www.ijera.com 3(5);420-424.
- [4] Suneeth Sukumaran et al. (2023). Experimental and finite element analysis of thermal stress on thermal spray coated AISI 304 stainless steel specimen using low cost solid lubricant. *International Journal on Interactive Design and Manufacturing*

- (IJIDeM) 18(5):1-11 DOI:10.1007/s12008-023-01322-8
- [5] Linfang Fang et al. (2024). Finite element (FE) analysis of thermal stress in production process of multi-layer lining ladle. *Case Studies in Thermal Engineering*. 57;104307.
- [6] Clemens Groth/Günter Müller. (2001). FEM fürPraktiker- Band 3. Temperataurfeld, 4.Auflage *Renningen-Malmsheim:expert-Verlag*.
- [7] O. Shorinov. (2022). Finite element analysis of thermal stress in Cu2O coating synthesized on Cu substrate. Archives of Materials Science and Engineering. 115(2);58-65 DOI:10.5604/01.3001.0016.0753.
- [8] Materials Data Book (2003). Cambridge University Engineering Department. http://www-mdp.eng.cam.ac.uk/web/library/enginfo/cueddatabooks/materials.pdf.
- [9] Naim Syla and Fisnik Aliaj. (2015). Finite-element modelling and experimental study of nitrogen concentration profile in 16MnCr5 gas nitrided steel. *Scientific Research and Essays*, 10(19), 615-623.
- [10] Kejun Hu.(2019). Simulation of Thermal Stress and Fatigue Life Prediction of High Speed Steel Work Roll during Hot Rolling Considering the Initial Residual Stress. *Metals*. 9(9), 966; https://doi.org/10.3390/met9090966
- [11]Taşkaya, S., Wu, D., Kurt, M., Liao, Y., Xu, J., & Liao, W. (2024). Exploring the Application of Building Information Modeling (BIM) in Town Planning: Key Roles in the Relationship Between Buildings and Parcels. *International Journal of Computational and Experimental Science and Engineering*, 10(4). https://doi.org/10.22399/iicesen.459
- [12]VURUR, T., & Recep KILIÇ. (2024). Design Optimization of Road Wheel Used in Tracked Armored Vehicles. *International Journal of Computational and Experimental Science and Engineering*, 10(4). https://doi.org/10.22399/ijcesen.798
- [13]Şen BAYKAL, D., Ghada ALMISNED, Hessa ALKARRANI, & H.O. TEKIN. (2024). Radiation Shielding Characteristics and Transmission Factor values of some Selected Alloys: A Monte Carlo-Based Study. *International Journal of Computational and Experimental Science and Engineering*, 10(4). https://doi.org/10.22399/ijcesen.421
- [14]Çalık, A., & Uçar, N. (2024). Microstructure properties of welded S420MC dual phase steel. *International Journal of Computational and Experimental Science and Engineering*, 10(2). https://doi.org/10.22399/ijcesen.336
- [15]Şen Baykal, D., ALMISNED, G., ALKARRANI, H., & TEKIN, H. O. (2024). Exploring gamma-ray and neutron attenuation properties of some high-density alloy samples through MCNP Monte Carlo code. *International Journal of Computational and Experimental Science and Engineering*, 10(3). https://doi.org/10.22399/ijcesen.422

[16]Nazim UCAR, Adnan CALIK, & ÖZDEMİR, A. F. (2024). Tensile properties and microstructure of AISI 430 ferritic stainless steel welded TIG method. *International Journal of Computational and Experimental Science and Engineering*, 10(4). https://doi.org/10.22399/ijcesen.699